

Flutter analysis of an extradosed bridge in Hungary

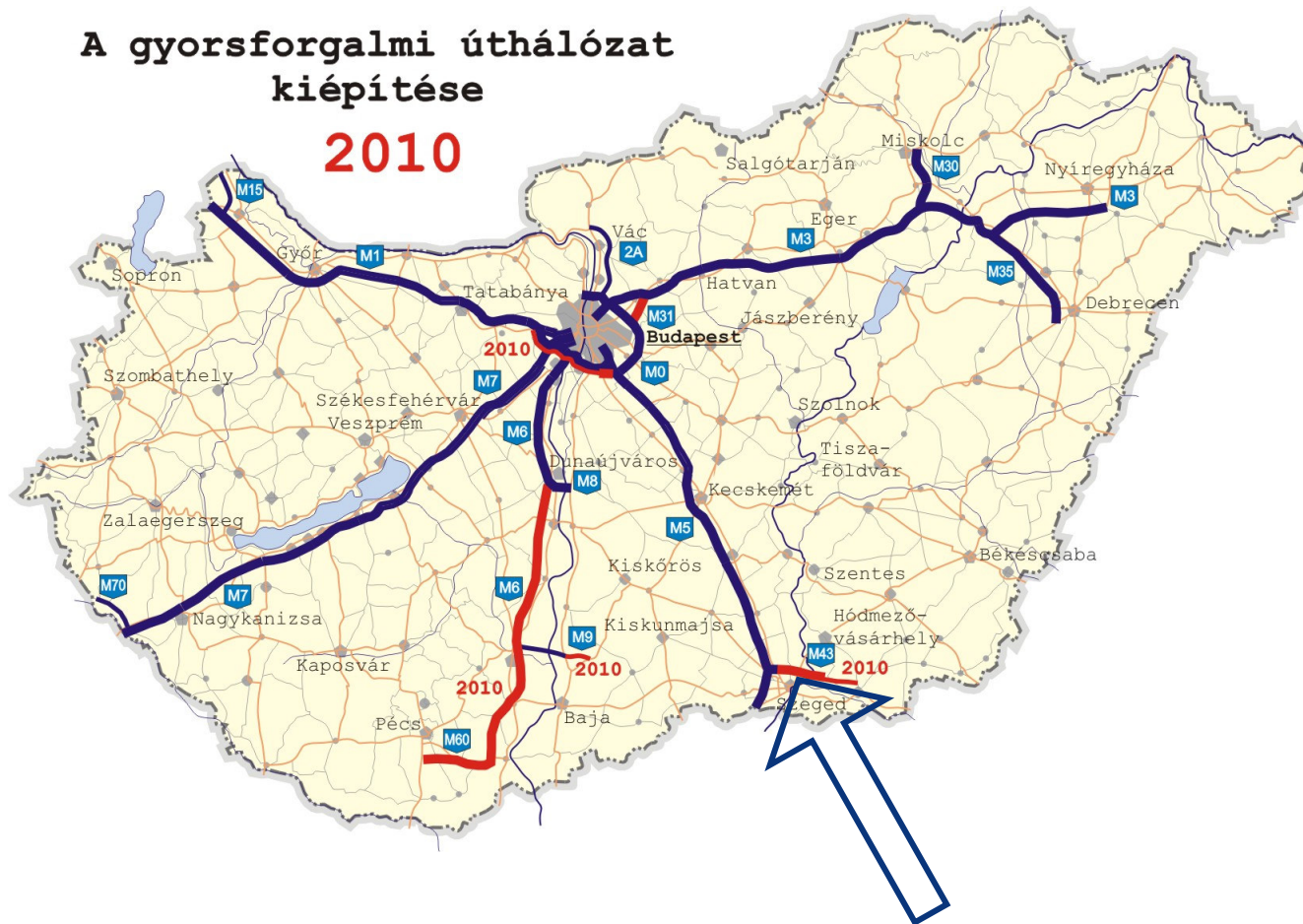
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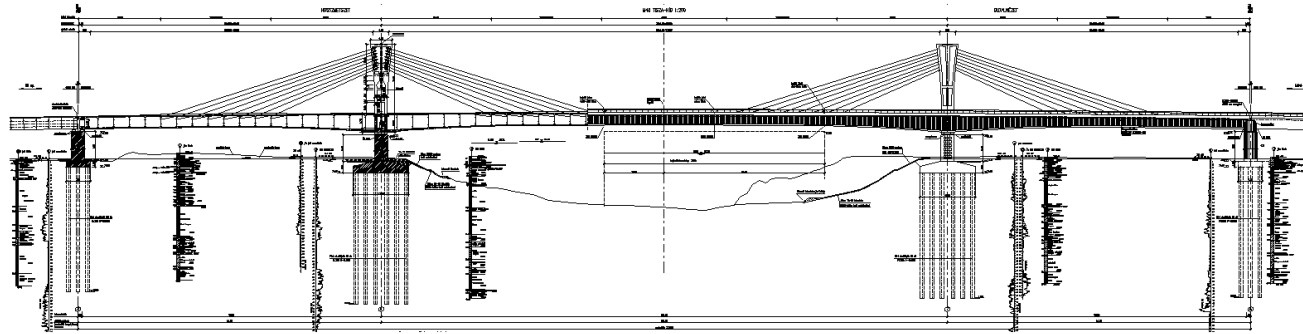
M43 motorway Tisza-bridge

A gyorsforgalmi úthálózat
kiépítése

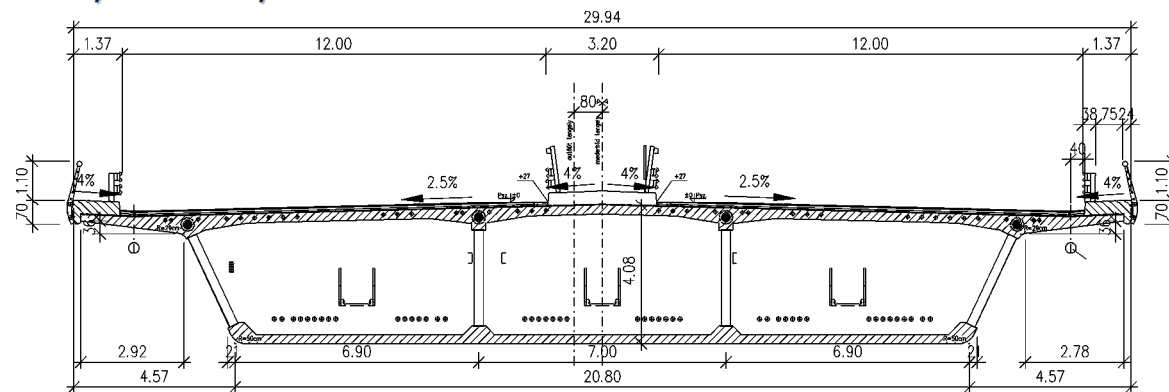
2010



M43 motorway Tisza-bridge



Spans: 96,30 + 180,00 + 96,30 m

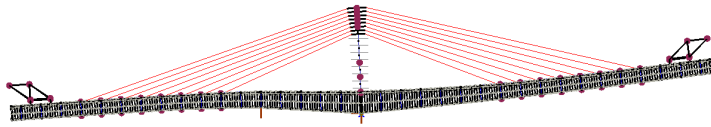


Courtesy of Pont-TERV

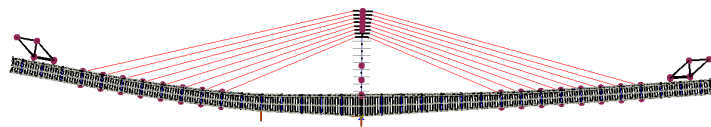
Flutter instability investigation:

- construction phase (cantilever stage)
- final phase

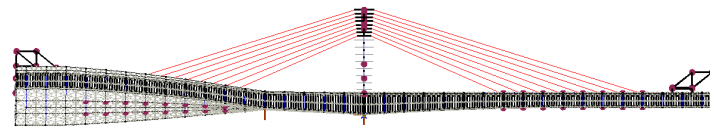
Mode shapes



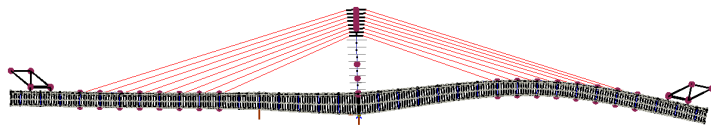
$n_1=0,55$ Hz



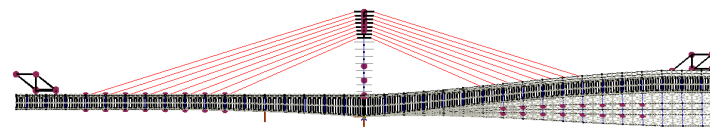
$n_2=0,78$ Hz



$n_7=2,47$ Hz



$n_6=2,33$ Hz

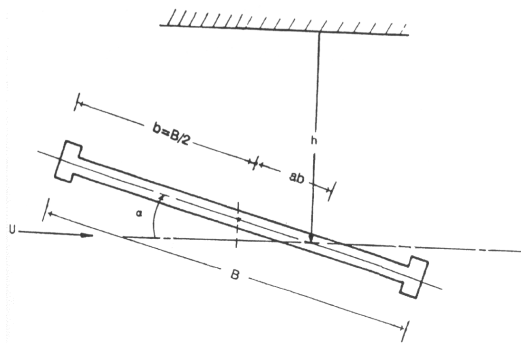


$n_8=2,80$ Hz

Szélhatások

- Kvázi-statikusan állapot
→ erőtenyező
- Dinamikus vizsgálat
→ átviteli függvény
- aeroelasztikus hatások
(öngerjesztett erők)
→ derivatívumok

Flutter analysis



- Middle-span cross section
- 2 DOF

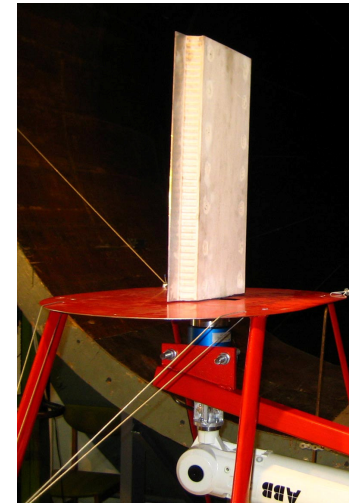
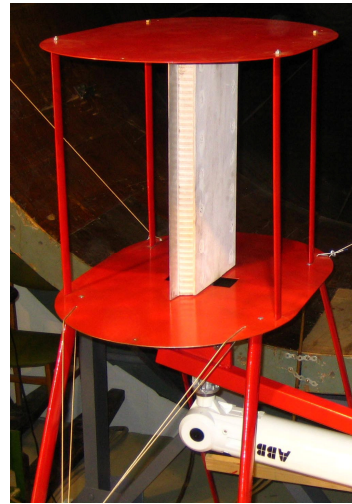
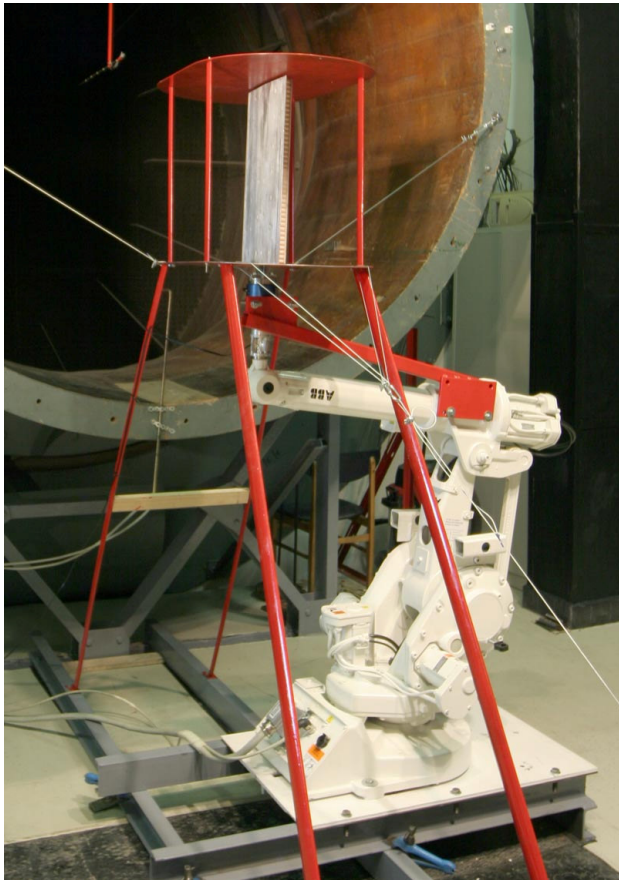
$$m\ddot{h} + c_h\dot{h} + k_h h = \frac{1}{2} \rho U^2 B \left(KH_1^*(K) \frac{\dot{h}}{U} + KH_2^*(K) \frac{B\dot{\alpha}}{U} + K^2 H_3^*(K) \alpha + K^2 H_4^* \frac{h}{B} \right)$$

$$S\ddot{\alpha} + c_\alpha \dot{\alpha} + k_\alpha \alpha = \frac{1}{2} \rho U^2 B^2 \left(KA_1^*(K) \frac{\dot{h}}{U} + KA_2^*(K) \frac{B\dot{\alpha}}{U} + K^2 A_3^*(K) \alpha + K^2 A_4^* \frac{h}{B} \right)$$

Instability criteria

- ω_{crit} , U_{crit}

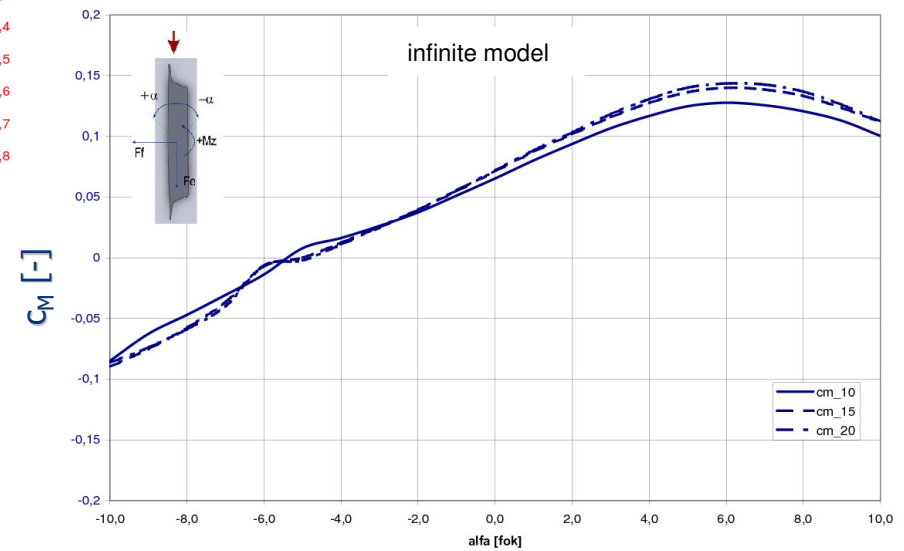
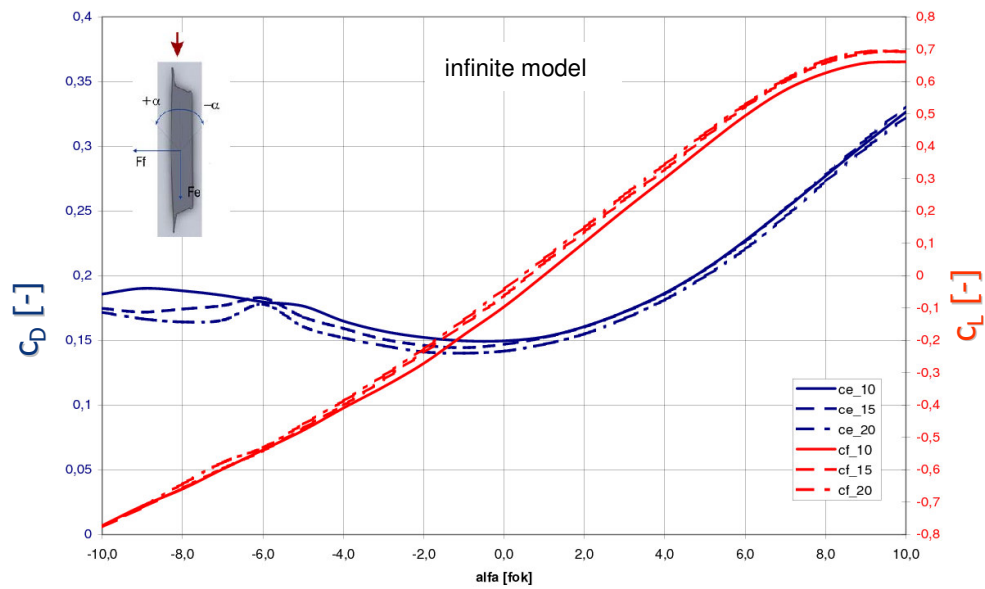
Wind tunnel investigation



- scale 1:100
- forced 2 DOF model
- semi-finite and infinite models
- angles of attack: -6° , 0° , $+6^\circ$
- small turbulent intensity ($I_u \leq 0,5\%$)
- separation of inertial forces, „no-wind” measures



Force coefficients

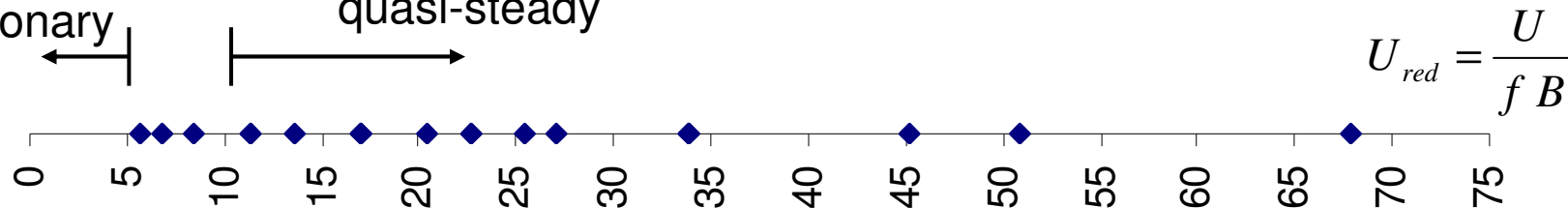


Wind tunnel investigation

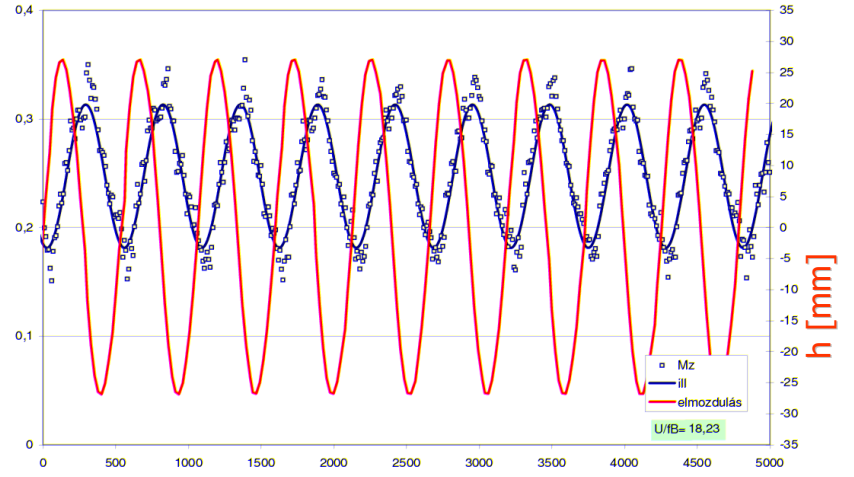
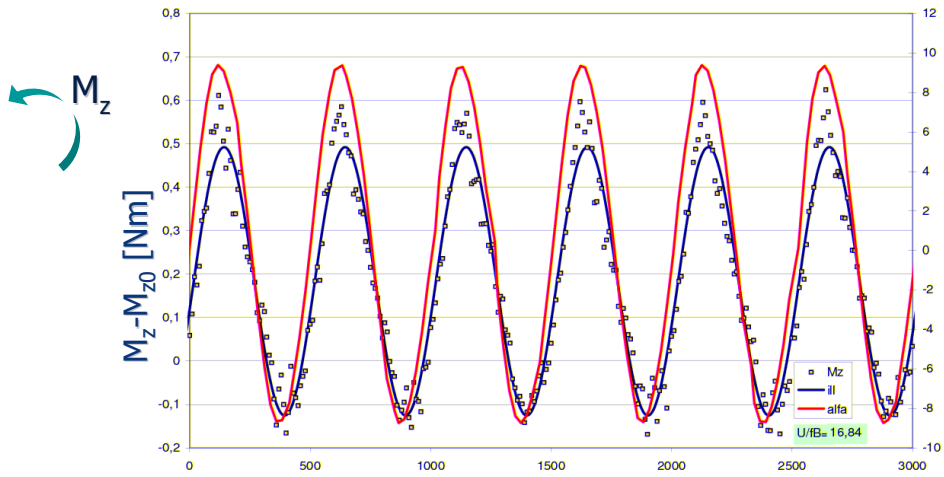
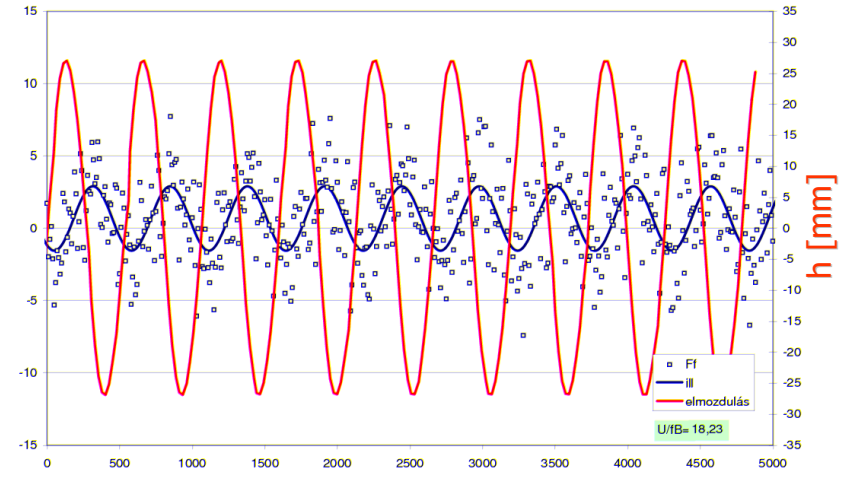
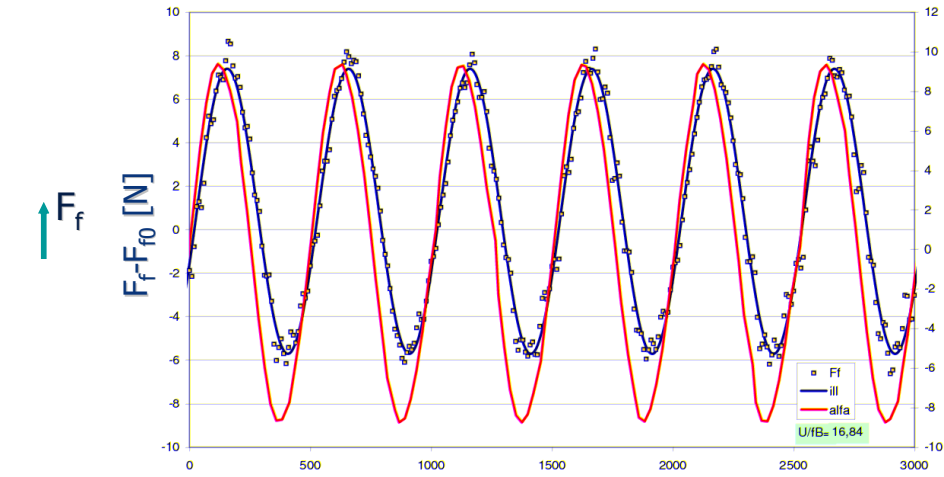
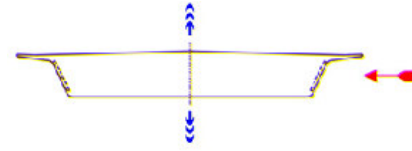
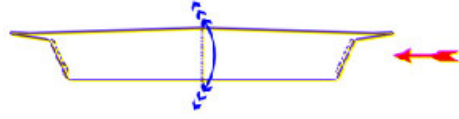
- motion frequency $f = 1,0; 1,5; 2,0; 2,5; 3,0$ Hz
- wind speed $U = 5; 10; 15; 20$ m/s
- model width $B = 295$ mm (scale 1:100)
- measuring by 6 dynamometers
- oscillation $\alpha = 0^\circ \pm 10^\circ$ $+6, -6 \pm 4^\circ$
 $h = \pm 30$ mm
- sampling rate 100 Hz

highly non-stationary

quasi-steady



$\alpha=0$ $f=2$ Hz $U=10$ m/s



t [ms]

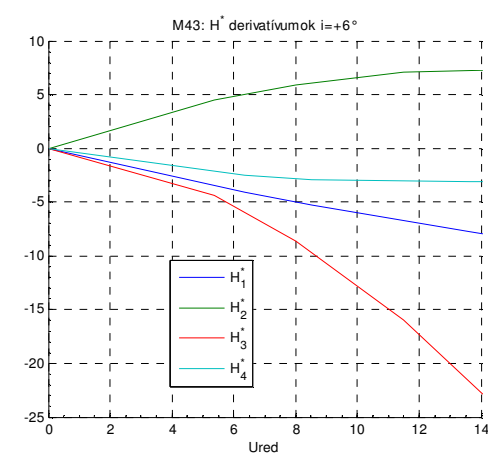
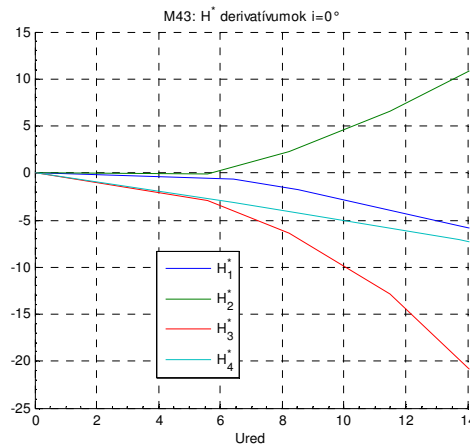
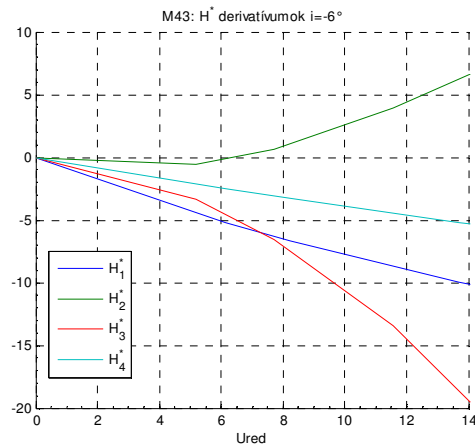
t [ms]

- measured force
- fitted curve
- displacement

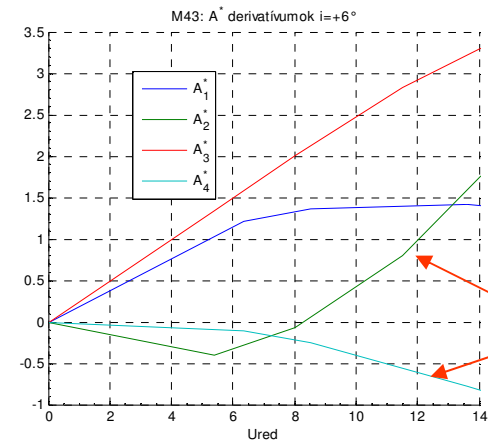
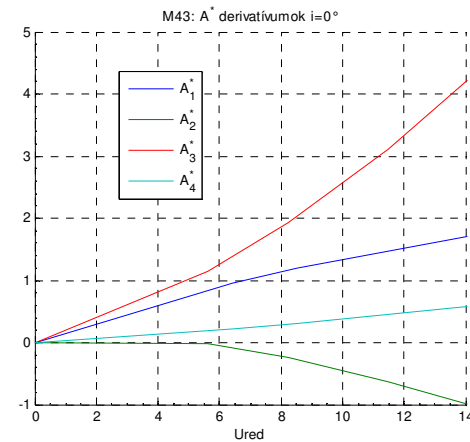
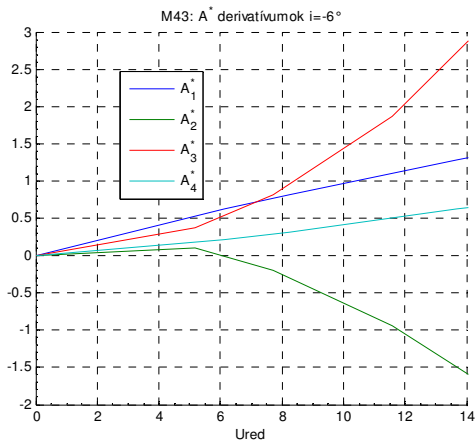
Flutter derivatives



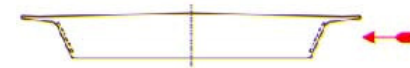
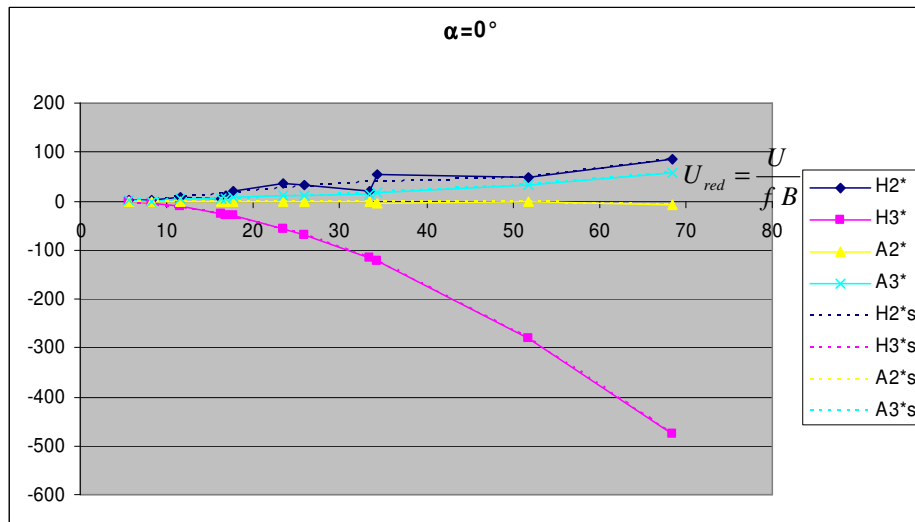
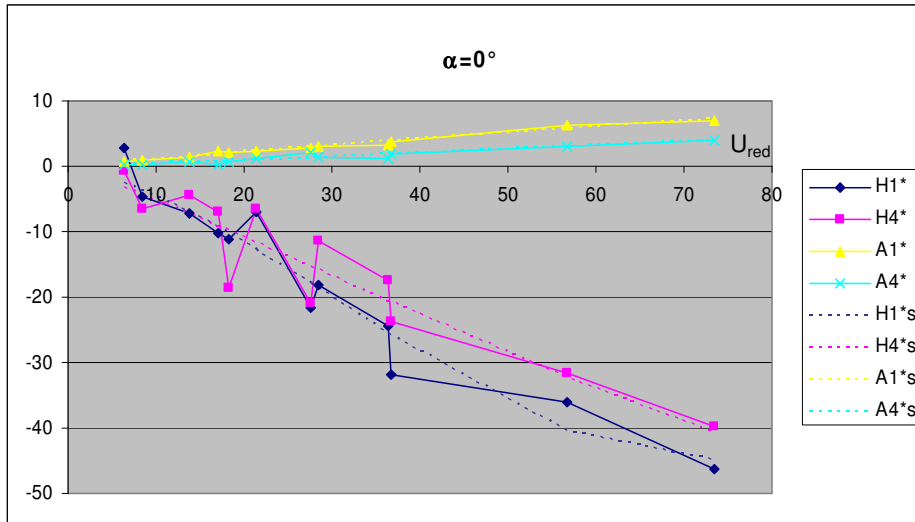
$L_h \uparrow$



M_α



Flutter derivatives



Polynomial fitting of 3rd order

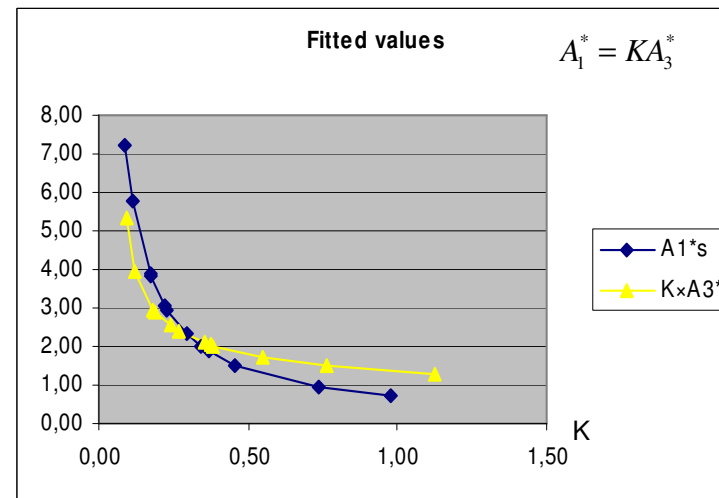
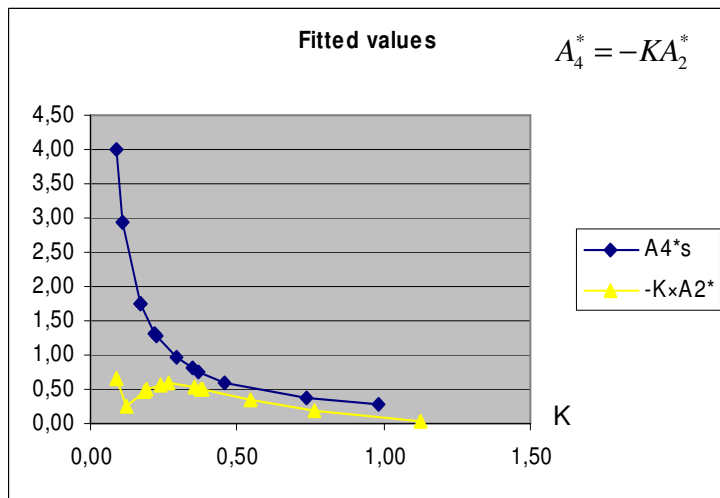
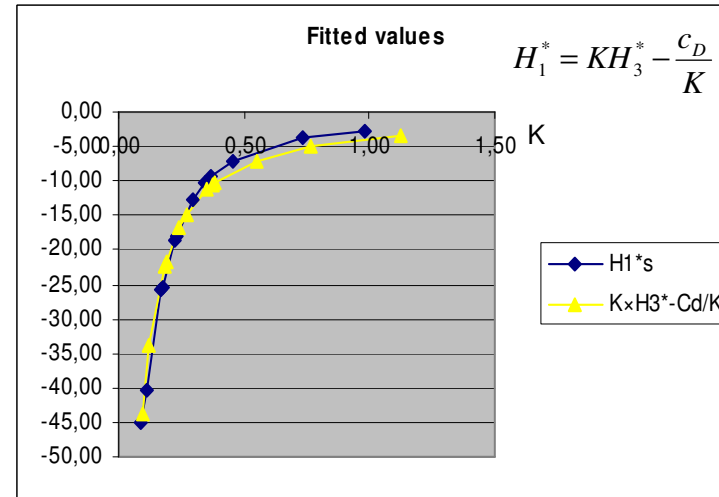
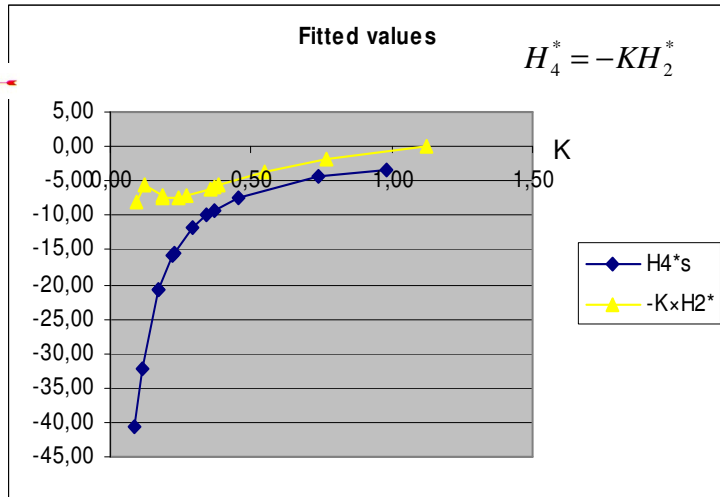
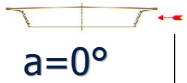
$$L_h = \frac{1}{2} \rho U^2 B \left(KH_1^*(K) \frac{\dot{h}}{U} + KH_2^*(K) \frac{B\dot{\alpha}}{U} + K^2 H_3^*(K) \alpha + K^2 H_4^* \frac{h}{B} \right)$$

$$M_\alpha = \frac{1}{2} \rho U^2 B^2 \left(KA_1^*(K) \frac{\dot{h}}{U} + KA_2^*(K) \frac{B\dot{\alpha}}{U} + K^2 A_3^*(K) \alpha + K^2 A_4^* \frac{h}{B} \right)$$

$$U_{red} = \frac{U}{fB} \quad K = \frac{2\pi f B}{U} = \frac{2\pi}{U_{red}}$$

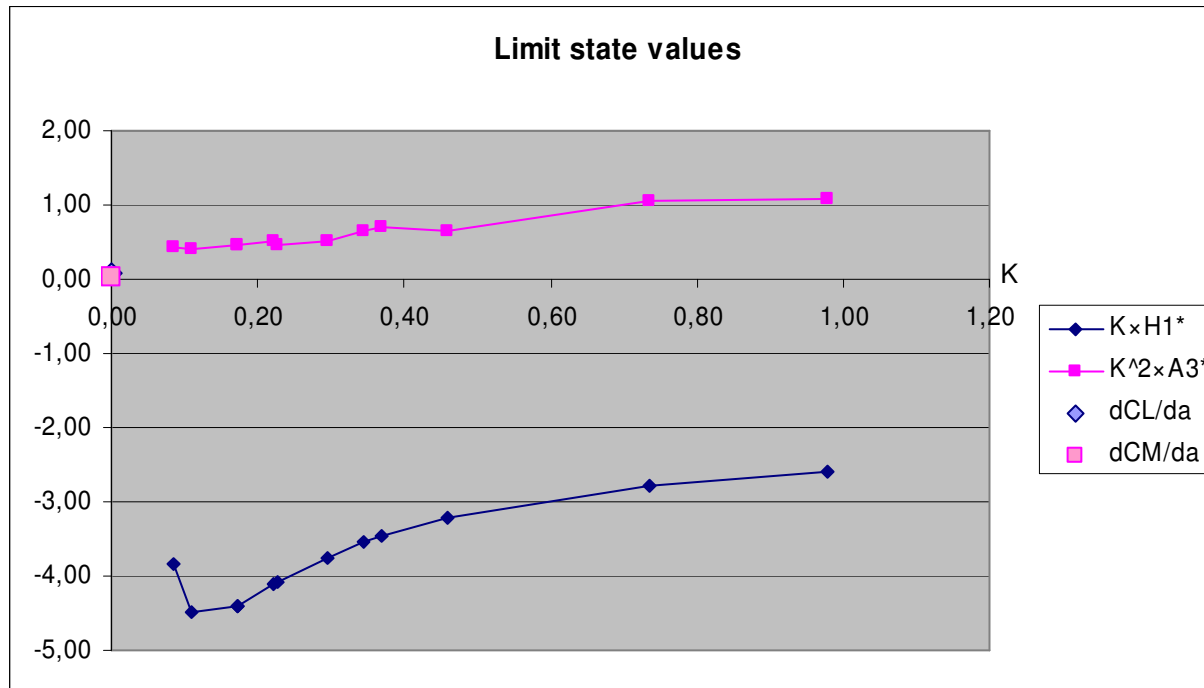
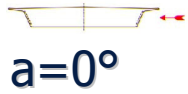
Polynomial fitting of 4th order

Verification



$$K = \frac{2\pi}{U_{red}}$$

Force coeffs. - derivatives

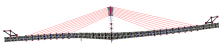

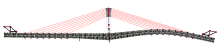
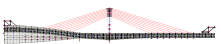


$$KH_1^* \xrightarrow{K \rightarrow 0} \frac{dc_L}{d\alpha}$$

$$K^2 A_3^* \xrightarrow{K \rightarrow 0} \frac{dc_M}{d\alpha}$$

Flutter condition

Damping factor: 3,5%

α [°]	f_B [1/s]	f_T [1/s]	Φ	$U_{red,crit}$ [-]	ω_{crit} [1/s]	U_{0crit} [m/s]
+6			1,00	0,59	3,47 *	12,87*
0	0,55	2,80		2,20	3,46 B	47,9
-6				0,62	14,40 T	56,12
+6			0,90	0,04	15,28 *	3,84*
0	2,33	2,47		2,45	15,30 B	226
-6				4,85	14,30 T	435

Affinity in the cross-terms: ΦA_1^* , ΦA_4^* , ΦH_2^* , ΦH_3^*

Max. wind speed

- Lack of wind map for Hungary → middle-Germany
- 10 min average wind velocity
- 20-30 oscillations for instability → duration of 5 sec
- $p=0,02$ annual probability of exceedence
- maximum wind speed 35,5 m/s
- safety against flutter instability $(U_{crit}/U_{max})^2 = (47,9/35,5)^2 = \mathbf{1,82}$

Conclusion

- Enough safety against flutter instability
- More measures in the highly non-stationary domain, at low reduced velocities
- Acceptable set-up, but a special test rig could be designed
- More verification during the wind tunnel test

Thank you for your kind attention

Acknowledgements

- dr. I. Hegedűs, BME
 - dr. I. Kovács, Dynamic-Consulting (BRD)
- for their comments and help in this work